

Table A for Sight-Reduction according to R. Doniol

degrees		<i>sin</i> cos	delta	degrees		<i>sin</i> cos	delta	<i>cot</i> tan	degrees		<i>sin</i> cos	delta	<i>cot</i> tan	degrees
90	0	100000	0.0	60	30	86603	14.5		30	60	50000	25.2	1.73	120
.	.	99996	0.3	.	.	86163	14.8		.	.	49242	25.3	1.77	.
89	1	99985	0.5	59	31	85717	15.0		29	61	48481	25.4	1.80	119
.	.	99966	0.8	.	.	85264	15.2		.	.	47716	25.6	1.84	.
88	2	99939	1.0	58	32	84805	15.4		28	62	46947	25.7	1.88	118
.	.	99905	1.3	.	.	84339	15.6		.	.	46175	25.8	1.92	.
87	3	99863	1.5	57	33	83867	15.8		27	63	45399	25.9	1.96	117
.	.	99813	1.8	.	.	83389	16.1		.	.	44620	26.0	2.01	.
86	4	99756	2.0	56	34	82904	16.3		26	64	43837	26.1	2.05	116
.	.	99692	2.3	.	.	82413	16.5		.	.	43051	26.3	2.10	.
85	5	99619	2.5	55	35	81915	16.7		25	65	42262	26.4	2.14	115
.	.	99540	2.8	.	.	81412	16.9		.	.	41469	26.5	2.19	.
84	6	99452	3.0	54	36	80902	17.1		24	66	40674	26.6	2.25	114
.	.	99357	3.3	.	.	80386	17.3		.	.	39875	26.7	2.30	.
83	7	99255	3.5	53	37	79864	17.5		23	67	39073	26.8	2.36	113
.	.	99144	3.8	.	.	79335	17.7		.	.	38268	26.9	2.41	.
82	8	99027	4.0	52	38	78801	17.9		22	68	37461	27.0	2.48	112
.	.	98902	4.3	.	.	78261	18.1		.	.	36650	27.1	2.54	.
81	9	98769	4.6	51	39	77715	18.3		21	69	35837	27.2	2.61	111
.	.	98629	4.8	.	.	77162	18.5		.	.	35021	27.2	2.67	.
80	10	98481	5.1	50	40	76604	18.7		20	70	34202	27.3	2.75	110
.	.	98325	5.3	.	.	76041	18.9		.	.	33381	27.4	2.82	.
79	11	98163	5.6	49	41	75471	19.1		19	71	32557	27.5	2.90	109
.	.	97992	5.8	.	.	74896	19.3		.	.	31730	27.6	2.99	.
78	12	97815	6.0	48	42	74314	19.5		18	72	30902	27.7	3.08	108
.	.	97630	6.3	.	.	73728	19.7		.	.	30071	27.7	3.17	.
77	13	97437	6.5	47	43	73135	19.8		17	73	29237	27.8	3.27	107
.	.	97237	6.8	.	.	72537	20.0		.	.	28402	27.9	3.38	.
76	14	97030	7.0	46	44	71934	20.2		16	74	27564	28.0	3.49	106
.	.	96815	7.3	.	.	71325	20.4		.	.	26724	28.0	3.61	.
75	15	96593	7.5	45	45	70711	20.6	1.00	15	75	25882	28.1	3.73	105
.	.	96363	7.8	.	.	70091	20.7	1.02	.	.	25038	28.2	3.87	.
74	16	96126	8.0	44	46	69466	20.9	1.04	14	76	24192	28.2	4.01	104
.	.	95882	8.3	.	.	68835	21.1	1.05	.	.	23345	28.3	4.17	.
73	17	95630	8.5	43	47	68200	21.3	1.07	13	77	22495	28.3	4.33	103
.	.	95372	8.7	.	.	67559	21.4	1.09	.	.	21644	28.4	4.51	.
72	18	95106	9.0	42	48	66913	21.6	1.11	12	78	20791	28.5	4.70	102
.	.	94832	9.2	.	.	66262	21.8	1.13	.	.	19937	28.5	4.92	.
71	19	94552	9.5	41	49	65606	22.0	1.15	11	79	19081	28.6	5.14	101
.	.	94264	9.7	.	.	64945	22.1	1.17	.	.	18224	28.6	5.40	.
70	20	93969	9.9	40	50	64279	22.3	1.19	10	80	17365	28.6	5.67	100
.	.	93667	10.2	.	.	63608	22.4	1.21	.	.	16505	28.7	5.98	.
69	21	93358	10.4	39	51	62932	22.6	1.23	9	81	15643	28.7	6.31	99
.	.	93042	10.7	.	.	62251	22.8	1.26	.	.	14781	28.8	6.69	.
68	22	92718	10.9	38	52	61566	22.9	1.28	8	82	13917	28.8	7.12	98
.	.	92388	11.1	.	.	60876	23.1	1.30	.	.	13053	28.8	7.60	.
67	23	92050	11.4	37	53	60182	23.2	1.33	7	83	12187	28.9	8.14	97
.	.	91706	11.6	.	.	59482	23.4	1.35	.	.	11320	28.9	8.78	.
66	24	91355	11.8	36	54	58779	23.5	1.38	6	84	10453	28.9	9.51	96
.	.	90996	12.1	.	.	58070	23.7	1.40	.	.	09585	29.0	10.39	.
65	25	90631	12.3	35	55	57358	23.8	1.43	5	85	08716	29.0	11.43	95
.	.	90259	12.5	.	.	56641	24.0	1.46	.	.	07846	29.0	12.71	.
64	26	89879	12.8	34	56	55919	24.1	1.48	4	86	06976	29.0	14.30	94
.	.	89493	13.0	.	.	55194	24.3	1.51	.	.	06105	29.0	16.35	.
63	27	89101	13.2	33	57	54464	24.4	1.54	3	87	05234	29.0	19.08	93
.	.	88701	13.4	.	.	53730	24.5	1.57	.	.	04362	29.1	22.90	.
62	28	88295	13.7	32	58	52992	24.7	1.60	2	88	03490	29.1	28.64	92
.	.	87882	13.9	.	.	52250	24.8	1.63	.	.	02618	29.1	38.19	.
61	29	87462	14.1	31	59	51504	24.9	1.66	1	89	01745	29.1	57.29	91
.	.	87036	14.3	.	.	50754	25.1	1.70	.	.	00873	29.1	114.59	.
60	30	86603	14.5	30	60	50000	25.2	1.73	0	90	00000	29.1		90

This is a reconstruction of the Table Robert Diniol originally published 1955 in conjunction with his compact Sight Reduction Methode in the journal "Revue Technique de Navigation Maritime et Aerienn".

Table B for Sight-Reduction according to R. Doniol

<i>h m s</i>	<i>f'</i>	<i>f</i>	<i>a</i>	<i>Pa</i>	<i>h m s</i>	<i>f'</i>	<i>f</i>	<i>a</i>	<i>Pa</i>		
<i>Pa</i>	<i>a</i>	<i>f</i>	<i>f'</i>	<i>h m s</i>	<i>Pa</i>	<i>a</i>	<i>f</i>	<i>f'</i>	<i>h m s</i>		
00 00 00	0.000			1.000	12 00 00	03 32 31	0.200	8.6	34.4	0.800	08 27 29
00 06 29	0.000	0.2	1215	1.000	11 53 31	03 35 22	0.205	8.7	33.8	0.795	08 24 38
00 10 15	0.001	0.4	769	1.000	11 49 45	03 38 12	0.210	8.9	33.3	0.790	08 21 48
00 14 30	0.001	0.5	543	0.999	11 45 30	03 41 00	0.215	9.0	32.8	0.785	08 19 00
00 20 30	0.002	0.8	384	0.998	11 39 30	03 43 47	0.220	9.1	32.4	0.780	08 16 13
00 25 07	0.003	0.9	313	0.997	11 34 53	03 46 32	0.225	9.3	31.9	0.775	08 13 28
00 29 01	0.004	1.1	271	0.996	11 30 59	03 49 16	0.230	9.4	31.5	0.770	08 10 44
00 32 26	0.005	1.2	242	0.995	11 27 34	03 51 59	0.235	9.5	31.0	0.765	08 08 01
00 35 32	0.006	1.3	221	0.994	11 24 28	03 54 40	0.240	9.7	30.6	0.760	08 05 20
00 38 24	0.007	1.4	205	0.993	11 21 36	03 57 21	0.245	9.8	30.2	0.755	08 02 39
00 41 03	0.008	1.5	191	0.992	11 18 57	04 00 00	0.250	9.9	29.8	0.750	08 00 00
00 43 33	0.009	1.6	180	0.991	11 16 27	04 02 38	0.255	10.1	29.4	0.745	07 57 22
00 45 55	0.010	1.7	171	0.990	11 14 05	04 05 16	0.260	10.2	29.0	0.740	07 54 44
00 48 10	0.011	1.8	163	0.989	11 11 50	04 07 52	0.265	10.3	28.6	0.735	07 52 08
00 52 23	0.013	2.0	150	0.987	11 07 37	04 10 27	0.270	10.5	28.3	0.730	07 49 33
00 56 17	0.015	2.1	139	0.985	11 03 43	04 13 02	0.275	10.6	27.9	0.725	07 46 58
00 59 56	0.017	2.3	131	0.983	11 00 04	04 15 35	0.280	10.7	27.6	0.720	07 44 25
01 03 23	0.019	2.4	124	0.981	10 56 37	04 18 08	0.285	10.9	27.2	0.715	07 41 52
01 06 39	0.021	2.5	117	0.979	10 53 21	04 20 40	0.290	11.0	26.9	0.710	07 39 20
01 09 47	0.023	2.6	112	0.977	10 50 13	04 23 11	0.295	11.1	26.6	0.705	07 36 49
01 12 47	0.025	2.8	107	0.975	10 47 13	04 25 41	0.300	11.3	26.3	0.700	07 34 19
01 15 40	0.027	2.9	103	0.973	10 44 20	04 28 11	0.305	11.4	25.9	0.695	07 31 49
01 19 48	0.030	3.0	98	0.970	10 40 12	04 30 40	0.310	11.5	25.6	0.690	07 29 20
01 23 44	0.033	3.2	93	0.967	10 36 16	04 33 08	0.315	11.7	25.3	0.685	07 26 52
01 27 30	0.036	3.3	89	0.964	10 32 30	04 35 36	0.320	11.8	25.1	0.680	07 24 24
01 31 07	0.039	3.5	85	0.961	10 28 53	04 38 03	0.325	11.9	24.8	0.675	07 21 57
01 34 36	0.042	3.6	82	0.958	10 25 24	04 40 30	0.330	12.1	24.5	0.670	07 19 30
01 37 59	0.045	3.7	79	0.955	10 22 01	04 42 55	0.335	12.2	24.2	0.665	07 17 05
01 41 15	0.048	3.9	77	0.952	10 18 45	04 45 21	0.340	12.3	23.9	0.660	07 14 39
01 44 25	0.051	4.0	74	0.949	10 15 35	04 47 46	0.345	12.5	23.7	0.655	07 12 14
01 47 30	0.054	4.1	72	0.946	10 12 30	04 50 10	0.350	12.6	23.4	0.650	07 09 50
01 51 29	0.058	4.3	69	0.942	10 08 31	04 52 34	0.355	12.8	23.2	0.645	07 07 26
01 55 21	0.062	4.4	67	0.938	10 04 39	04 54 58	0.360	12.9	22.9	0.640	07 05 02
01 59 06	0.066	4.6	65	0.934	10 00 54	04 57 21	0.365	13.0	22.7	0.635	07 02 39
02 02 44	0.070	4.7	63	0.930	09 57 16	04 59 43	0.370	13.2	22.4	0.630	07 00 17
02 06 17	0.074	4.9	61	0.926	09 53 43	05 02 05	0.375	13.3	22.2	0.625	06 57 55
02 09 44	0.078	5.0	59	0.922	09 50 16	05 04 27	0.380	13.5	22.0	0.620	06 55 33
02 13 07	0.082	5.1	58	0.918	09 46 53	05 06 49	0.385	13.6	21.7	0.615	06 53 11
02 16 25	0.086	5.3	56	0.914	09 43 35	05 09 10	0.390	13.7	21.5	0.610	06 50 50
02 19 40	0.090	5.4	55	0.910	09 40 20	05 11 31	0.395	13.9	21.3	0.605	06 48 29
02 23 37	0.095	5.6	53	0.905	09 36 23	05 13 51	0.400	14.0	21.1	0.600	06 46 09
02 27 29	0.100	5.7	52	0.900	09 32 31	05 16 11	0.405	14.2	20.8	0.595	06 43 49
02 31 15	0.105	5.9	50	0.895	09 28 45	05 18 31	0.410	14.3	20.6	0.590	06 41 29
02 34 57	0.110	6.0	49	0.890	09 25 03	05 20 51	0.415	14.5	20.4	0.585	06 39 09
02 38 35	0.115	6.2	48	0.885	09 21 25	05 23 10	0.420	14.6	20.2	0.580	06 36 50
02 42 09	0.120	6.3	47	0.880	09 17 51	05 25 30	0.425	14.8	20.0	0.575	06 34 30
02 45 38	0.125	6.5	45	0.875	09 14 22	05 27 49	0.430	14.9	19.8	0.570	06 32 11
02 49 04	0.130	6.6	44	0.870	09 10 56	05 30 07	0.435	15.1	19.6	0.565	06 29 53
02 52 27	0.135	6.8	44	0.865	09 07 33	05 32 26	0.440	15.2	19.4	0.560	06 27 34
02 55 47	0.140	6.9	43	0.860	09 04 13	05 34 44	0.445	15.4	19.2	0.555	06 25 16
02 59 04	0.145	7.1	42	0.855	09 00 56	05 37 03	0.450	15.5	19.0	0.550	06 22 57
03 02 18	0.150	7.2	41	0.850	08 57 42	05 39 21	0.455	15.7	18.8	0.545	06 20 39
03 05 29	0.155	7.4	40	0.845	08 54 31	05 41 39	0.460	15.9	18.6	0.540	06 18 21
03 08 38	0.160	7.5	39	0.840	08 51 22	05 43 57	0.465	16.0	18.4	0.535	06 16 03
03 11 44	0.165	7.6	39	0.835	08 48 16	05 46 14	0.470	16.2	18.3	0.530	06 13 46
03 14 48	0.170	7.8	38	0.830	08 45 12	05 48 32	0.475	16.3	18.1	0.525	06 11 28
03 17 50	0.175	7.9	37	0.825	08 42 10	05 50 50	0.480	16.5	17.9	0.520	06 09 10
03 20 50	0.180	8.1	37	0.820	08 39 10	05 53 07	0.485	16.7	17.7	0.515	06 06 53
03 23 48	0.185	8.2	36	0.815	08 36 12	05 55 25	0.490	16.8	17.5	0.510	06 04 35
03 26 44	0.190	8.3	35	0.810	08 33 16	05 57 42	0.495	17.0	17.4	0.505	06 02 18
03 29 39	0.195	8.5	35	0.805	08 30 21	06 00 00	0.500	17.2	17.2	0.500	06 00 00

This is a reconstruction of the Table Robert Diniol originally published 1955 in conjunction with his compact Sight Reduction Methode in the journal "Revue Technique de Navigation Maritime et Aerienne".

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